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(54) Catalyst for purifying exhaust gases.

(57) A catalyst for purifying exhaust gases includes a support including at least one composite selected from the group consisting of $\text{TiO}_2\text{-Al}_2\text{O}_3$, $\text{ZrO}_2\text{-Al}_2\text{O}_3$ and $\text{SiO}_2\text{-Al}_2\text{O}_3$ composites, an NO_x adsorbent including at least one member selected from the group consisting of alkali metals, alkaline-earth metals and rare-earth elements and loaded on the support, and a noble metal catalyst ingredient loaded on the support. The composites constituting the support improve initial NO_x conversion of the catalyst, but also inhibit NO_x purifying performance thereof from degrading even after a durability test.

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BACKGROUND OF THE INVENTIONField of the Invention

5 The present invention relates to a catalyst for purifying exhaust gases. More particularly, it relates to the catalyst which can efficiently purify nitrogen oxides (NO_x) in the exhaust gases whose oxygen concentrations are at the stoichiometric point or more than required for oxidizing carbon monoxide (CO) and hydrocarbons (HC) therein.

10 Description of Related Art

As catalysts for purifying automotive exhaust gases, there have been employed 3-way catalysts so far which oxidize CO and HC and reduce NO_x to purify the exhaust gases. For example, the 3-way catalysts have been known widely which comprise a heat resistant support formed of cordierite, a catalyst carrier layer formed of gamma-alumina and disposed on the support, and a noble metal catalyst ingredient selected from the group consisting of Pt, Pd and Rh and loaded on the catalyst carrier layer.

The purifying performance of the 3-way catalysts for purifying exhaust gases depends greatly on the air-fuel ratio A/F of automotive engine. For instance, when the air-fuel weight ratio is larger than 14.6, i.e., when the fuel concentration is low (or on the fuel-lean side), the oxygen concentration is high in exhaust gases. Accordingly, the oxidation reactions purifying CO and HC are active, but the reduction reactions purifying NO_x are inactive. On the other hand, when the air-fuel ratio is smaller than 14.6, i.e., when the fuel concentration is higher (or on the fuel-rich side), the oxygen concentration is low in exhaust gases. Accordingly, the oxidation reactions are inactive, but the reduction reactions are active.

Moreover, when driving automobiles, especially when driving automobiles in urban areas, the automobiles are accelerated and decelerated frequently. Consequently, the air-fuel ratio varies frequently in the range of from the values adjacent to the stoichiometric point (or the theoretical air-fuel ratio: 14.6) to the fuel-rich side. In order to satisfy the low fuel consumption requirement during the driving conditions such as in the above-described urban areas, it is necessary to operate the automobiles on the fuel-lean side where the air-fuel mixture containing oxygen as excessive as possible is supplied to the engines. Hence, it has been desired to develop a catalyst which is capable of adequately purifying NO_x even on the fuel-lean side (i.e., in the oxygen-rich atmospheres).

In view of the aforementioned circumstances, the applicants et al. of the present invention proposed a novel catalyst in Japanese Unexamined Patent Publication (KOKAI) No. 5-317,652. This catalyst comprises an alkaline-earth metal oxide and Pt which are loaded on its porous support. In the catalyst, during the fuel-lean side (i.e., in the oxygen-rich atmospheres) driving, NO_x is adsorbed on the alkaline-earth metal elements, and it reacts with the reducing gas such as HC and the like to be purified. As a result, the catalyst exhibits superb NO_x purifying performance during the fuel-lean side (i.e., in the oxygen-rich atmospheres) driving.

The catalyst proposed in Japanese Unexamined Patent Publication (KOKAI) No. 5-317,652 is believed to provide the advantageous effect as follows: the alkaline-earth metals are loaded on the support in the form of their simple oxides, for example, barium oxide, and they react with NO_x to produce nitrates, e.g., $\text{Ba}(\text{NO}_3)_2$. Thus, NO_x is adsorbed on the support of the catalyst in the form of the alkaline-earth metal nitrates.

In addition, as set forth in Japanese Unexamined Patent Publication (KOKAI) Nos. 5-168,860 and 6-31,139, exhaust-gases-purifying catalysts have been known in which an NO_x adsorbent and Pt or the like are loaded on a heat resistant inorganic oxide. The NO_x adsorbent includes barium representing alkaline-earth metals, or lanthanum representing rare-earth elements. The heat resistant inorganic oxide includes zeolite, alumina or the like.

However, the exhaust gases usually contain SO_x which is produced by burning sulfur (S) contained in the fuel. Further, the catalyst ingredient oxidizes SO_x to SO_3 in the oxygen-rich atmospheres (i.e., on the fuel-lean side). Still further, SO_3 reacts readily with water vapor also contained in the exhaust gases to produce sulfuric acid. It has been revealed that the resulting sulfuric acid reacts with the alkaline-earth metal elements to produce alkaline-earth metal sulfites and alkaline-earth metal sulfates, thereby poisoning the alkaline-earth metal elements (i.e., NO_x adsorbent). Moreover, the porous support made of alumina, etc., is likely to adsorb SO_x , thereby facilitating the poisoning.

Specifically, when the NO_x adsorbent, such as alkaline-earth metal elements, is turned into the sulfites and sulfates, it hardly adsorbs NO_x thereon. As a result, the catalyst proposed in Japanese Unexamined Patent Publication (KOKAI) No. 5-317,652 might suffer from a drawback in that it is deteriorated in terms of

the NO_x purifying performance after it is subjected to a durability test.

In addition, titania (TiO₂) does not adsorb SO_x thereon. Hence, the inventors of the present invention thought of employing a support made of titania, and carried out a series of experiments. As a result, they found that, in a catalyst comprising a titania support, SO_x is not adsorbed but flows as it is to a downstream side, and that only the SO_x which contacts directly with a noble metal catalyst ingredient is oxidized. Thus, they revealed that the poisoning develops less. However, they also discovered that the catalyst comprising the titania support has a detrimental characteristic in that it exhibits low initial purifying activity and keeps low NO_x purifying performance after a durability test.

10 SUMMARY OF THE INVENTION

The present invention has been developed in view of the aforementioned circumstances. It is therefore an object of the present invention to provide a catalyst which can not only exhibit satisfactory initial NO_x conversion securely but also can inhibit its NO_x purifying performance even after a durability test.

15 In accordance with a first aspect of the present invention, a catalyst can solve the aforementioned problems. A catalyst according to the first aspect of the present invention comprises:

a support including at least one composite selected from the group consisting of TiO₂-Al₂O₃, ZrO₂-Al₂O₃ and SiO₂-Al₂O₃ composites;

an NO_x adsorbent including at least one member selected from the group consisting of alkali metals, alkaline-earth metals and rare-earth elements, and loaded on the support; and
20 a noble metal catalyst ingredient loaded on the support.

In accordance with a second aspect of the present invention, a catalyst can also solve the aforementioned problems. A catalyst according to the second aspect of the present invention comprises:

a composite support including TiO₂, Al₂O₃, and at least one element selected from the group consisting of alkaline-earth metals and rare-earth elements;
25 of alkaline-earth metals and rare-earth elements;

an NO_x adsorbent including at least one member selected from the group consisting of alkali metals, alkaline-earth metals and rare-earth elements, and loaded on the composite support; and
a noble metal catalyst ingredient loaded on the composite support.

Unless otherwise specified, the term, "rare-earth elements," herein includes not only the chemical elements with atomic numbers 58 through 71, but also ²¹Sc, ³⁹Y and ⁵⁷La.

In the catalyst according to the first aspect of the present invention, the support is employed which includes at least one composite selected from the group consisting of TiO₂-Al₂O₃, ZrO₂-Al₂O₃ and SiO₂-Al₂O₃ composites. This arrangement apparently enables to effect advantages of TiO₂, ZrO₂, SiO₂ and Al₂O₃ only, though reasons behind the advantageous operation is still under investigation.

35 Specifically, the advantages of Al₂O₃ enhance initial NO_x conversion. Compared with Al₂O₃, TiO₂, ZrO₂ and SiO₂ are less likely to adsorb SO_x. Even when they adsorb SO_x, they are more likely to release SO_x at low temperatures than the NO_x adsorbent. Thus, they are inhibited from being poisoned by SO_x. As a result, when the present catalyst employs the composites as its support, the present catalyst can exhibit satisfactory initial NO_x conversion securely. Moreover, SO_x is inhibited from adsorbing on the present catalyst, and consequently the present catalyst can exhibit improved NO_x conversion even after a durability test.

Hereinafter, TiO₂, ZrO₂ and SiO₂ employed in the catalyst according to the first aspect of the present invention are collectively referred to as MO₂. When amounts of MO₂ and Al₂O₃ are defined by moles of their metallic components, compositing ratio of MO₂ with respect to Al₂O₃ (i.e., M/Al expressed in molar ratio) preferably satisfies the following relationship:
45

$$M/Al = 5/95 \text{ through } 50/50.$$

When the compositing ratio M/Al is smaller than 5/95, the resulting catalysts exhibit deteriorated NO_x conversion after a durability test. When the compositing ratio M/Al is larger than 50/50, the resulting catalysts exhibit deteriorated initial NO_x conversion and exhibit poor NO_x conversion, degrading according to the enlarging compositing ratio M/Al, after a durability test. It is especially preferable that the compositing ratio M/Al satisfies the following relationship:

55 $M/Al = 20/80 \text{ through } 30/70.$

In addition, it is preferred that MO₂ and Al₂O₃ are composited at level as small as possible. That is, it is preferable to make MO₂ and Al₂O₃ into composite oxide than to simply mixing them, and it is further

preferable to composite them at atomic level. In order to composite them at atomic level, a coprecipitation process, a sol-gel process and the like are available.

In the catalyst according to the second aspect of the present invention, the composite support is employed which includes TiO_2 , Al_2O_3 , and at least one element selected from the group consisting of
5 alkaline-earth elements and rare earth elements.

In particular, when a catalyst employs a composite support including TiO_2 - Al_2O_3 composite, it was discovered that TiO_2 facilitates to transform Al_2O_3 into α - Al_2O_3 and to deteriorate the resulting catalysts in terms of purifying performance, especially oxidation activity. Further, it was found that Al_2O_3 is facilitated to transform into α - Al_2O_3 according to increasing TiO_2 content. However, when a TiO_2 - Al_2O_3 composite
10 is further composited with one of alkaline-earth elements and rare earth elements or with both of them, a catalyst employing a support made of such a composite can be inhibited from degrading in terms of oxidation activity after a durability test and accordingly can exhibit high purifying performance. Reasons behind this advantageous operation is unknown, and is still under investigation.

As for the support or the composite support, it is possible to prepare it in any form, e.g., a honeycomb-
15 formed support made from at least one of the composites, a honeycomb-formed support made from cordierite and coated with at least one of the composites, and a honeycomb-formed support made from heat resistant metal and coated with at least one of the composites.

As for the NO_x adsorbent, it is possible to employ at least one element selected from the group consisting of alkali metals, alkaline-earth metals and rare earth elements. As for the alkali metals, the
20 following elements are available: lithium (Li), sodium (Na), potassium (K), rubidium (Rb), cesium (Cs) and francium (Fr). The term, "alkaline-earth metals," herein means the elements of group 2A in the periodic table of the elements. For instance, the following elements are available: barium (Ba), beryllium (Be), magnesium (Mg), calcium (Ca) and strontium (Sr). As for the rare earth elements, the following elements are available: scandium (Sc), yttrium (Y), lanthanum (La), cerium (Ce), praseodymium (Pr) and neodymium
25 (Nb).

The loading amount of the NO_x adsorbent preferably falls in a range of from 0.05 to 1.0 mole with respect to 120 grams of the support or the composite support. When it is less than 0.05 moles with respect thereto, the resulting catalysts exhibit small NO_x adsorbing capability and deteriorate in terms of NO_x purifying performance. When it is more than 1.0 mole, not only the advantageous effects resulting from the
30 NO_x adsorbent saturate but also there arise the other problems resulting from the reduced loading amount of the noble metal catalyst ingredient.

As for the noble metal catalyst ingredient, it is possible at least one element selected from the group consisting of Pt, Rh and Pd. When Pt or Pd is loaded, it is preferably loaded in an amount of from 0.1 to 20.0 grams with respect to 120 grams of the support or the composite support, further preferably in an
35 amount of from 0.5 to 10.0 grams with respect thereto. When Rh is loaded, it is preferably loaded in an amount of from 0.01 to 80.0 grams with respect to 120 grams of the support or the composite support, further preferably in an amount of from 0.05 to 5.0 grams with respect thereto. These loading amounts of the noble metal catalyst ingredient can be converted into values with respect to the unit volume (e.g., 1 liter) of the support or the composite support. For example, when Pt or Pd is loaded, it is preferably loaded in an
40 amount of from 0.1 to 20.0 grams with respect to 1 liter of the support or the composite support, further preferably in an amount of from 0.5 to 10.0 grams with respect thereto. When Rh is loaded, it is preferably loaded in an amount of from 0.01 to 80.0 grams with respect to 1 liter of the support or the composite support, further preferably in an amount of from 0.05 to 5.0 grams with respect thereto.

Thus, in accordance with the first aspect of the present invention, the catalyst can securely exhibit
45 satisfactory initial NO_x conversion. Moreover, SO_x is inhibited from adsorbing on the present catalyst, and consequently from poisoning the NO_x adsorbent. As a result, the present catalyst can exhibit improved NO_x conversion which is inhibited from deteriorating even after a durability test.

The second aspect of the present invention operates and provides advantageous effects identically with the first aspect of the present invention. In addition, when a TiO_2 - Al_2O_3 composite is employed to make the
50 support of the present catalyst, the present catalyst can be inhibited from degrading in terms of oxidation activity after a durability test, and accordingly can exhibit highly-maintained CO and HC purifying performance.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

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Having generally described the present invention, a further understanding can be obtained by reference to the specific preferred embodiments which are provided herein for purposes of illustration only and are not intended to limit the scope of the appended claims.

Unless otherwise specified, the term, "parts," hereinafter means "parts by weight."

First Preferred Embodiment

5 (Preparation of $\text{TiO}_2\text{-Al}_2\text{O}_3$ Composite Powder)

3 liters of 2-propanol was charged into a flask adapted for synthesizing sol-gel and provided with a reflux, and it was held at 80°C . While stirring the 2-propanol, 1,225 grams of aluminum isopropoxide was charged into the flask to dissolve, and the mixed solution was further stirred at 80°C for 2 hours.

10 Thereafter, while stirring the mixed solution at 80°C , 189.6 grams of tetraethyl titanate was dropped into the flask. After dropping all of the tetraethyl titanate, the mixed solution was further kept to be stirred at 80°C for 2 hours.

Moreover, while stirring the mixed solution at 80°C , a mixed solution containing 432 grams of pure water and 2 liters of 2-propanol was dropped. The dropping rate was adjusted to 20 c.c./min. After dropping, 15 the mixed solution was kept to be stirred at 80°C for 2 hours.

Finally, after aging the thus mixed solution at room temperature for one day and one night, the water content and the alcohol content were removed from the mixed solution by using a rotary evaporator. After naturally drying the resulting residue, the residue was dried forcibly at 110°C , and it was calcinated at 600°C for 3 hours. Thus, a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 20 9.6/90.4 expressed in molar ratio.

(Noble Metal Catalyst Ingredient Loading)

With respect to 120 grams of the resulting $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder, a platinum dinitrodiamine 25 aqueous solution was impregnated in a predetermined amount. The composite powder undergone the impregnation was dried at 110°C , and thereafter it was calcinated at 250°C for 1 hour. The loading amount of Pt was 2.0 grams with respect to 120 grams of the composite powder.

(NO_x Adsorbent Loading)

30 With respect to the resulting $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder with Pt loaded, a barium acetate aqueous solution was impregnated in a predetermined amount. The composite powder with Pt loaded undergone the impregnation was dried at 110°C , and thereafter it was calcinated at 500°C for 3 hours. The loading amount of Ba was 0.3 moles with respect to 120 grams of the composite powder.

35 The thus produced composite powder with Pt and Ba loaded was formed into a preform by applying pressure. The preform was then pulverized, thereby preparing pellet-shaped catalysts of the First Preferred Embodiment.

Second Preferred Embodiment

40 Except that a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 25/75 expressed in molar ratio, pellet-shaped catalysts of the Second Preferred Embodiment were prepared in the same manner as the First Preferred Embodiment.

45 Third Preferred Embodiment

Except that a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 50/50 expressed in molar ratio, pellet-shaped catalysts of the Third Preferred Embodiment were prepared in the same manner as the First Preferred Embodiment.

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Fourth Preferred Embodiment

Except that a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 70/30 expressed in molar ratio, pellet-shaped catalysts of the Fourth Preferred Embodiment were prepared in the 55 same manner as the First Preferred Embodiment.

Fifth Preferred Embodiment

In the Fifth Preferred Embodiment, a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al
compositing ratio of 25/75 expressed in molar ratio. After loading Pt in the same manner as the First
Preferred Embodiment, a sodium acetate aqueous solution, instead of the barium acetate aqueous solution,
was impregnated. The composite powder undergone the impregnation was dried at 110°C , and it was
calcinated at 500°C for 3 hours. The loading amount of Na was 0.3 moles with respect to 120 grams of the
composite powder.

The thus produced composite powder with Pt and Na loaded was formed into a preform by applying
pressure. The preform was then pulverized, thereby preparing pellet-shaped catalysts of the Fifth Preferred
Embodiment.

Sixth Preferred Embodiment

Except that a potassium acetate aqueous solution was used instead of the sodium acetate aqueous
solution to load K, instead of Na, in a loading amount of 0.3 moles with respect to 120 grams of the
composite powder, pellet-shaped catalysts of the Sixth Preferred Embodiment were prepared in the same
manner as the Fifth Preferred Embodiment.

Seventh Preferred Embodiment

Except that a cesium nitrate aqueous solution was used instead of the sodium acetate aqueous solution
to load Cs, instead of Na, in a loading amount of 0.3 moles with respect to 120 grams of the composite
powder, pellet-shaped catalysts of the Seventh Preferred Embodiment were prepared in the same manner
as the Fifth Preferred Embodiment.

Comparative Example No. 1

Except that a $\gamma\text{-Al}_2\text{O}_3$ powder was used instead of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder, pellet-
shaped catalysts of Comparative Example No. 1 were prepared in the same manner as the First Preferred
Embodiment.

Comparative Example No. 2

Except that a TiO_2 powder was used instead of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder, pellet-shaped
catalysts of Comparative Example No. 2 were prepared in the same manner as the First Preferred
Embodiment.

Examination and Evaluation

Each of the pellet-shaped catalysts of the First through Seventh Preferred Embodiments and Compara-
tive Example Nos. 1 and 2 was examined for initial NO_x conversion as well as NO_x conversion after a
durability test. The results of this examination are set forth in Table 1 below.

The initial NO_x conversion was examined by using a model gas which simulated an exhaust gas emitted
from an automobile engine. Specifically, it was examined when the automobile engine was operated
alternately under 2 conditions, namely when the automobile engine was operated alternately at an A/F ratio
of 18 for 2 minutes and at an A/F ratio of 14 for 2 minutes.

TABLE 1

	Support Composition (Compositing Ratio)	Pt Loading Amount (grams/liter)	NOx Adsorbent Loading (mole/liter)	Initial NOx Conversion (%)	NOx Conversion after Durability Test (%)
1st Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=9.6/90.4)	2.0	0.3 (Ba)	71	39
2nd Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=25/75)	2.0	0.3 (Ba)	62	54
3rd Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=50/50)	2.0	0.3 (Ba)	48	34
4th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=70/30)	2.0	0.3 (Ba)	38	20
5th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=25/75)	2.0	0.3 (Na)	72	64
6th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=25/75)	2.0	0.3 (K)	75	66
7th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (Ti/Al=25/75)	2.0	0.3 (Cs)	73	63
Comp. Ex. No. 1	gamma-Al ₂ O ₃	2.0	0.3 (Ba)	80	41
Comp. Ex. No. 2	TiO ₂	2.0	0.3 (Ba)	32	30

The NO_x conversion after a durability test was examined by using a first model gas which was equivalent to a fuel-air mixture having an A/F ratio of 18 and which had an SO₂ concentration of 300 ppm, and by using a second model gas which was equivalent to a fuel-air mixture having an A/F ratio of 14. Specifically, the first model gas was flowed through the pellet-shaped catalysts at 600 °C for 20 hours, and thereafter the second model gas was flowed through them at 600 °C for 1 hour. Each of the thus degraded

pell t-shaped catalysts was examined for its NO_x conversion in the same manner as the above-described initial NO_x conversion examination, -thereby examining the catalysts for the NO_x conversion after a durability test.

It is understood from Table 1 that, when observing the degradation of the NO_x conversion after a durability test with respect to the initial NO_x conversion, the exhaust-gases-purifying catalysts of the First through Seventh Preferred Embodiment degraded less than those of Comparative Example No. 1 did. Thus, the exhaust-gases-purifying catalysts of the First through Seventh Preferred Embodiments employing the composite supports were apparently improved over those of Comparative Example No. 1 employing the simple alumina support in terms of durability.

In addition, when the Ti/Al compositing ratio was around 25/75, the exhaust-gases-purifying catalysts of the First through Seventh Preferred Embodiments exhibited the maximum NO_x conversion after a durability test which exceeded the value exhibited by Comparative Example No. 1 (i.e., the novel catalyst proposed in Japanese Unexamined Patent Publication (KOKAI) No. 5-317,652). Since they did not exhibit maximum in the initial NO_x conversion, it is believed that the maximum value in the NO_x conversion after a durability test is effected, not by simply mixing TiO₂ and Al₂O₃, but by synergetic effect which results from compositing TiO₂ and Al₂O₃.

Note that, although the exhaust-gases-purifying catalysts of Comparative Example No. 2 exhibited a small difference between the initial NO_x conversion and the NO_x conversion after a durability test, they exhibited a low initial NO_x conversion and consequently they exhibited a lowered NO_x conversion after a durability test.

Eighth Preferred Embodiment

(Preparation of ZrO₂-Al₂O₃ Composite Powder)

3 liters of 2-propanol was charged into a flask adapted for synthesizing sol-gel and provided with a reflux, and it was held at 80 °C. While stirring the 2-propanol, 1,000 grams of aluminum isopropoxide was charged into the flask to dissolve, and the mixed solution was further stirred at 80 °C for 2 hours.

Thereafter, while stirring the mixed solution, 245.3 grams of a zirconium n-butoxide solution having a concentration of 85% by weight was dropped into the flask. After dropping all of the zirconium n-butoxide solution, the mixed solution was further kept to be stirred at 80 °C for 2 hours.

Moreover, while stirring the mixed solution at 80 °C, a mixed solution containing 432 grams of pure water and 2 liters of 2-propanol was dropped. The dropping rate was adjusted to 20 c.c./min. After dropping, the mixed solution was kept to be stirred at 80 °C for 2 hours.

Finally, after aging the thus mixed solution at room temperature for one day and one night, the water content and the alcohol content were removed from the mixed solution by using a rotary evaporator. After naturally drying the resulting residue, the residue was dried forcibly at 110 °C, and it was calcinated at 600 °C for 3 hours. Thus, a ZrO₂-Al₂O₃ composite powder was produced which had a Zr/Al compositing ratio of 1/9 expressed in molar ratio.

(Noble Metal Catalyst Ingredient Loading)

With respect to 120 grams of the resulting ZrO₂-Al₂O₃ composite powder, a platinum dinitrodiammine aqueous solution was impregnated in a predetermined amount. The composite powder undergone the impregnation was dried at 110 °C, and thereafter it was calcinated at 250 °C for 1 hour. The loading amount of Pt was 2.0 grams with respect to 120 grams of the composite powder. Further, a rhodium nitrate aqueous solution was impregnated in a predetermined amount. The composite powder undergone this second impregnation was dried at 110 °C, and thereafter it was calcinated at 250 °C for 1 hour. The loading amount of Rh was 0.1 gram with respect to 120 grams of the composite powder.

(NO_x Adsorbent Loading)

With respect to the resulting ZrO₂-Al₂O₃ composite powder with Pt and Rh loaded, a barium acetate aqueous solution was impregnated in a predetermined amount. The composite powder with Pt and Rh loaded undergone this impregnation was dried at 110 °C, and thereafter it was calcinated at 500 °C for 3 hours. The loading amount of Ba was 0.3 moles with respect to 120 grams of the composite powder.

The thus produced composite powder with Pt, Rh and Ba loaded was formed into a preform by applying pressure. The preform was then pulverized, thereby preparing pellet-shaped catalysts of the

Eighth Preferred Embodiment.

Ninth Preferred Embodiment

- 5 Except that a $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Zr/Al compositing ratio of 1/3 expressed in molar ratio, pellet-shaped catalysts of the Ninth Preferred Embodiment were prepared in the same manner as the Eighth Preferred Embodiment.

Tenth Preferred Embodiment

- 10 Except that a $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Zr/Al compositing ratio of 1/1 expressed in molar ratio, pellet-shaped catalysts of the Tenth Preferred Embodiment were prepared in the same manner as the Eighth Preferred Embodiment.

15 Eleventh Preferred Embodiment

Except that a $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Zr/Al compositing ratio of 2/1 expressed in molar ratio, pellet-shaped catalysts of the Eleventh Preferred Embodiment were prepared in the same manner as the Eighth Preferred Embodiment.

20 Twelfth Preferred Embodiment

- 25 Except that a $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Zr/Al compositing ratio of 1/1 expressed in molar ratio, and that a potassium acetate aqueous solution, instead of the barium acetate aqueous solution, was impregnated to load K in a loading amount of 0.3 moles with respect to 120 grams of the composite powder, pellet-shaped catalysts of the Twelfth Preferred Embodiment were prepared in the same manner as the Eighth Preferred Embodiment.

Comparative Example No. 3

- 30 Except that a gamma- Al_2O_3 powder was used instead of the $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder, pellet-shaped catalysts of Comparative Example No. 3 were prepared in the same manner as the Eighth Preferred Embodiment.

35 Comparative Example No. 4

Except that a ZrO_2 powder was used instead of the $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder, pellet-shaped catalysts of Comparative Example No. 4 were prepared in the same manner as the Eighth Preferred Embodiment.

40 Comparative Example No. 5

- 45 Except that a gamma- Al_2O_3 powder was used instead of the $\text{ZrO}_2\text{-Al}_2\text{O}_3$ composite powder, and that a potassium acetate aqueous solution, instead of the barium acetate aqueous solution, was impregnated to load K in a loading amount of 0.3 moles with respect to 120 grams of the composite powder, pellet-shaped catalysts of Comparative Example No. 5 were prepared in the same manner as the Eighth Preferred Embodiment.

Examination and Evaluation

- 50 Each of the pellet-shaped catalysts of the Eighth through Twelfth Preferred Embodiments and Comparative Example Nos. 3 through 5 was examined for initial NO_x conversion as well as NO_x conversion after a durability test. The results of this examination are set forth in Table 2 below.

- 55 The initial NO_x conversion was examined by using a model gas which simulated an exhaust gas emitted from an automobile engine. Specifically, it was examined when the automobile engine was operated alternately under 2 conditions, namely when the automobile engine was operated alternately at an A/F ratio of 18 for 2 minutes and at an A/F ratio of 14 for 2 minutes.

The NO_x conversion after a durability test was measured by using a first model gas which was equivalent to a fuel-air mixture having an A/F ratio of 18 and which had an SO₂ concentration of 300 ppm, and by using a second model gas which was equivalent to a fuel-air mixture having an A/F ratio of 14. Specifically, the first model gas was flowed through the pellet-shaped catalysts at 600 °C for 20 hours, and thereafter the second model gas was flowed through them at 600 °C for 1 hour. Each of the thus degraded pellet-shaped catalysts was examined for its NO_x conversion in the same manner as the above-described initial NO_x conversion examination, thereby examining the catalysts for the NO_x conversion after a durability test.

Moreover, a durability ratio R (%) was calculated by the following equation and also recited in Table 2:

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Durability Ratio R (%) = (Conversion after a Durability Test)/(Initial Conversion).

As can be appreciated from Table 2, when the exhaust-gases-purifying catalysts of the Eighth through Twelfth Preferred Embodiments employed the ZrO₂-Al₂O₃ composite supports, they exhibited initial NO_x conversion lowered with respect to those of Comparative Example Nos. 3 and 5. However, they exhibited the durability ratio R which exceeded those of Comparative Example Nos. 3 and 5. Thus, they were apparently improved over those of Comparative Example Nos. 3 through 5 in terms of durability.

In addition, when the Zr/Al compositing ratio was around 1/1, the exhaust-gases-purifying catalysts of the Eighth through Twelfth Preferred Embodiments exhibited their maximum durability.

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TABLE 2

	Support Composition (Compositing Ratio)	Pt Load- ing Amount (grams/ liter)	Rh Load- ing Amount (grams/ liter)	NOx Adsor- bent Loading Amount (mole/liter)	Initial NOx Conversion (%)	NOx Conversion after Durabi- lity Test (%)	Durabi- lity Ratio (%)
8th Pref. Embodiment	ZrO ₂ -Al ₂ O ₃ (Zr/Al=1/3)	2.0	0.1	0.3 (Ba)	78	47	60.0
9th Pref. Embodiment	ZrO ₂ -Al ₂ O ₃ (Zr/Al=1/3)	2.0	0.1	0.3 (Ba)	65	48	73.8
10th Pref. Embodiment	ZrO ₂ -Al ₂ O ₃ (Zr/Al=1/1)	2.0	0.1	0.3 (Ba)	63	53	82.5
11th Pref. Embodiment	ZrO ₂ -Al ₂ O ₃ (Zr/Al=2/1)	2.0	0.1	0.3 (Ba)	52	34	65.4
12th Pref. Embodiment	ZrO ₂ -Al ₂ O ₃ (Zr/Al=1/1)	2.0	0.1	0.3 (K)	66	54	81.8
Comp. Ex. No. 3	gamma-Al ₂ O ₃	2.0	0.1	0.3 (Ba)	80	41	51.3
Comp. Ex. No. 4	ZrO ₂	2.0	0.1	0.3 (Ba)	42	20	47.6
Comp. Ex. No. 5	gamma-Al ₂ O ₃	2.0	0.1	0.3 (K)	82	44	53.7

Thirteenth Preferred Embodiment(Preparation of $\text{SiO}_2\text{-Al}_2\text{O}_3$ Composite Powder)

5 3 liters of 2-propanol was charged into a flask adapted for synthesizing sol-gel and provided with a reflux, and it was held at 80 °C. While stirring the 2-propanol, 1,000 grams of aluminum isopropoxide was charged into the flask to dissolve, and the mixed solution was further stirred at 80 °C for 2 hours.

Thereafter, while stirring the mixed solution at 80 °C, 42.4 grams of tetraethyl orthosilicate was dropped into the flask. After dropping all of the tetraethyl orthosilicate, the mixed solution was further kept to be stirred at 80 °C for 2 hours.

10 Moreover, while stirring the mixed solution at 80 °C, a mixed solution containing 432 grams of pure water and 2 liters of 2-propanol was dropped. The dropping rate was adjusted to 20 c.c./min. After dropping, the mixed solution was kept to be stirred at 80 °C for 2 hours.

Finally, after aging the thus mixed solution at room temperature for one day and one night, the water content and the alcohol content were removed from the mixed solution by using a rotary evaporator. After naturally drying the resulting residue, the residue was dried forcibly at 110 °C, and it was calcinated at 600 °C for 3 hours. Thus, an $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had an Si/Al compositing ratio of 4/96 expressed in molar ratio.

20 (Coating Layer Forming)

100 parts of the composite powder, 70 parts of alumina sol containing alumina in an amount of 10% by weight, 15 parts of an aluminum nitrate aqueous solution containing aluminum nitrate in an amount of 40% by weight, and 30 parts of water were mixed, thereby preparing a slurry for coating. Then, a plurality of honeycomb support substrates formed of cordierite and having a volume of 1.7 liters were immersed into the slurry, and thereafter each of them was blown to blow away the slurry in excess. Each of the support substrates was dried at 80 °C for 20 minutes, and thereafter each of them was calcinated at 600 °C for 1 hour, thereby forming an $\text{SiO}_2\text{-Al}_2\text{O}_3$ coating layer thereon. The coating layer was thus coated on the honeycomb support substrate in an amount of 120 grams with respect to 1 liter of the honeycomb support substrate.

(Noble Metal Catalyst Ingredient Loading)

Each of the honeycomb support substrates having the coating layer was immersed into a platinum dinitrodiamine aqueous solution having a predetermined concentration, and thereafter it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Pt thereon. The loading amount of Pt was 2.0 grams with respect to 120 grams of the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite coating layer (or 1 liter of the honeycomb support substrate).

40 (NO_x Adsorbent Loading)

Then, each of the honeycomb support substrates with Pt loaded was immersed into a barium acetate aqueous solution having a predetermined concentration, and it was dried at 110 °C. After drying, each of them was calcinated at 600 °C for 1 hour. The loading amount of Ba was 0.3 moles with respect to 120 grams of the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite coating layer (or 1 liter of the honeycomb support substrate).

Fourteenth Preferred Embodiment

50 Except that an $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had an Si/Al compositing ratio of 10/90 expressed in molar ratio, catalysts of the Fourteenth Preferred Embodiment were prepared in the same manner as the Thirteenth Preferred Embodiment.

Fifteenth Preferred Embodiment

55 Except that an $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had an Si/Al compositing ratio of 20/80 expressed in molar ratio, catalysts of the Fifteenth Preferred Embodiment were prepared in the same manner as the Thirteenth Preferred Embodiment.

Sixteenth Preferred Embodiment

Except that an $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had an Si/Al compositing ratio of 35/65 expressed in molar ratio, catalysts of the Sixteenth Preferred Embodiment were prepared in the same manner as the Thirteenth Preferred Embodiment.

Seventeenth Preferred Embodiment

Except that an $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had an Si/Al compositing ratio of 50/50 expressed in molar ratio, catalysts of the Seventeenth Preferred Embodiment were prepared in the same manner as the Thirteenth Preferred Embodiment.

Eighteenth Preferred Embodiment

Except that a potassium acetate aqueous solution, instead of the barium acetate aqueous solution, was used to load K, instead of Ba, in a loading amount of 0.3 moles with respect to 120 grams of the composite powder, catalysts of the Eighteenth Preferred Embodiment were prepared in the same manner as the Thirteenth Preferred Embodiment.

Comparative Example No. 6

Except that a gamma- Al_2O_3 powder was used instead of the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder, catalysts of Comparative Example No. 6 were prepared in the same manner as the Thirteenth Preferred Embodiment.

Comparative Example No. 7

Except that an SiO_2 powder was used instead of the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder, catalysts of Comparative Example No. 7 were prepared in the same manner as the Thirteenth Preferred Embodiment.

Comparative Example No. 8

Except that a gamma- Al_2O_3 powder was used instead of the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite powder, and that a potassium acetate aqueous solution, instead of the barium acetate aqueous solution, was used to load K in a loading amount of 0.3 moles with respect to 120 grams of the composite powder, catalysts of Comparative Example No. 8 were prepared in the same manner as the Thirteenth Preferred Embodiment.

Examination and Evaluation

Each of the catalysts of the Thirteenth through Eighteenth Preferred Embodiments and Comparative Example Nos. 6 through 8 was disposed in an exhaust line of an actual vehicle equipped with a lean burn engine. The lean burn engine had a displacement of 1.6 liters. The vehicle was driven in the urban area running mode, for instance, it was alternately driven in the 10-mode for a certain period of time and then in the 15-mode for another certain period of time, thereby examining the catalysts for the conversion of CO, HC and NO_x .

After the aforementioned examination, each of the catalysts of the Thirteenth through Eighteenth Preferred Embodiments and Comparative Example Nos. 6 through 8 was subjected to a bench test on durability which utilized the same type of engine as above. Namely, each of them was disposed in an exhaust line of the engine, and then the engine was run for 50 hours while adjusting the temperature of the exhaust gas introduced into them at 650 °C at an air-fuel ratio A/F of 18. After this bench test was over, each of them was again disposed in the exhaust line of the actual vehicle. The vehicle was driven in the same manner as described above, thereby examining the catalysts for the conversion of CO, HC and NO_x . Note that, in order to facilitate the sulfur poisoning, the purified fuel contained sulfur in an amount of 70 ppm. The results of these examinations are summarized in the columns designated at "Initial Conversion" and "Conversion after Durability Test" in Table 3, respectively.

It is appreciated from Table 3 that, although the catalysts of the Thirteenth through Eighteenth Preferred Embodiments were inferior to those of Comparative Example Nos. 6 and 8 in terms of the initial NO_x conversion, they degraded in lesser degree in terms of the NO_x conversion after a durability test than those of Comparative Example Nos. 6 and 8 did. Thus, the catalysts of the Thirteenth through Eighteenth

Preferred Embodiments exhibited good durability.

When comparing the catalysts of Comparative Example No. 6 with those of Comparative Example No. 8, it is understood that the catalysts employing the gamma-Al₂O₃ coating layer with K loaded thereon exhibited degraded oxidation activity with respect to the catalysts employing the gamma-Al₂O₃ coating layer with Ba loaded. However, when comparing the catalysts of the Thirteenth Preferred Embodiment with those of the Eighteenth Preferred Embodiment, in the catalysts of the Eighteenth Preferred Embodiment in which K was loaded on the SiO₂-Al₂O₃ composite coating layer, the oxidation activity was enhanced equal to those of the Thirteenth Preferred Embodiment in which Ba was loaded on the SiO₂-Al₂O₃ composite coating layer.

In addition, it can be seen from Table 3 that the Si/Al compositing ratio preferably falls in a range of from 4/96 to 20/80, further preferably in a range of from 4/96 to 15/85.

TABLE 3

	Coating Layer Composition (Compositing Ratio)	Pt Loading Amount (grams/liter)	NOx Adsorbent Loading (mole/liter)	Initial Conversion (%)	Conversion after Durability Test (%)
				NOx HC CO	NOx HC CO
13th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=4/96)	2.0	0.3 (Ba)	76 99 100	64 89 99
14th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=10/90)	2.0	0.3 (Ba)	62 99 100	56 90 98
15th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=20/80)	2.0	0.3 (Ba)	52 98 100	46 90 98
16th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=35/65)	2.0	0.3 (Ba)	45 97 100	39 92 99
17th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=50/50)	2.0	0.3 (Ba)	40 97 100	34 90 98
18th Pref. Embodiment	SiO ₂ -Al ₂ O ₃ (Si/Al=4/96)	2.0	0.3 (K)	78 96 100	66 88 96
Comp. Ex. No. 6	gamma-Al ₂ O ₃	2.0	0.3 (Ba)	93 95 100	50 88 98
Comp. Ex. No. 7	SiO ₂	2.0	0.3 (Ba)	20 94 100	16 90 96
Comp. Ex. No. 8	gamma-Al ₂ O ₃	2.0	0.3 (K)	94 89 96	49 81 88

Nineteenth Preferred Embodiment(Preparation of $\text{TiO}_2\text{-Al}_2\text{O}_3\text{-Sc}_2\text{O}_3$ Composite Powder)

3 liters of 2-propanol was charged into a flask adapted for synthesizing sol-gel and provided with a reflux, and it was held at 80 °C. While stirring the 2-propanol, 1,225 grams of aluminum isopropoxide was charged into the flask to dissolve, and the mixed solution was further stirred at 80 °C for 2 hours.

Thereafter, while stirring the mixed solution at 80 °C, 568.4 grams of tetraethyl titanate was dropped into the flask. After dropping all of the tetraethyl titanate, the mixed solution was further kept to be stirred at 80 °C for 2 hours.

Moreover, while stirring the mixed solution at 80 °C, a mixed solution containing 432 grams of pure water and 2 liters of 2-propanol was dropped. The dropping rate was adjusted to 20 c.c./min. After dropping, the mixed solution was kept to be stirred at 80 °C for 2 hours.

Finally, after aging the thus mixed solution at room temperature for one day and one night, the water content and the alcohol content were removed from the mixed solution by using a rotary evaporator. After naturally drying the resulting residue, the residue was dried forcibly at 110 °C, and it was calcinated at 600 °C for 3 hours. Thus, a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 25/75 expressed in molar ratio.

In addition, into the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder, a scandium nitrate aqueous solution having a predetermined concentration was impregnated in a predetermined amount. The $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder with scandium nitrate impregnated was dried, and thereafter it was calcinated at 600 °C for 3 hours, thereby preparing a $\text{TiO}_2\text{-Al}_2\text{O}_3\text{-Sc}_2\text{O}_3$ composite powder. 0.013 moles of Sc_2O_3 was included therein with respect to 120 grams of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder.

(Coating Layer Forming)

100 parts of the composite powder, 70 parts of alumina sol containing alumina in an amount of 10% by weight, 15 parts of an aluminum nitrate aqueous solution containing aluminum nitrate in an amount of 40% by weight, and 30 parts of water were mixed, thereby preparing a slurry for coating. Then, a plurality of honeycomb support substrates formed of cordierite and having a volume of 1.7 liters were immersed into the slurry, and thereafter each of them was blown to blow away the slurry in excess. Each of the support substrates was dried at 80 °C for 20 minutes, and thereafter each of them was calcinated at 600 °C for 1 hour, thereby forming a $\text{TiO}_2\text{-Al}_2\text{O}_3\text{-Sc}_2\text{O}_3$ coating layer thereon. The coating layer was thus coated on the honeycomb support substrate in an amount of 120 grams with respect to 1 liter of the honeycomb support substrate.

(Noble Metal Catalyst Ingredient Loading)

Each of the honeycomb support substrates having the coating layer was immersed into a platinum dinitrodiammine aqueous solution having a predetermined concentration, and thereafter it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Pt thereon. The loading amount of Pt was 2.0 grams with respect to 120 grams of the $\text{TiO}_2\text{-Al}_2\text{O}_3\text{-Sc}_2\text{O}_3$ composite coating layer (or 1 liter of the honeycomb support substrate).

(NO_x Adsorbent Loading)

Then, each of the honeycomb support substrates with Pt loaded was immersed into a barium acetate aqueous solution having a predetermined concentration, and it was dried at 110 °C. After drying, each of them was calcinated at 600 °C for 1 hour. The loading amount of Ba was 0.3 moles with respect to 120 grams of the $\text{TiO}_2\text{-Al}_2\text{O}_3\text{-Sc}_2\text{O}_3$ composite coating layer (or 1 liter of the honeycomb support substrate).

Twentieth Preferred Embodiment

Except that an yttrium nitrate aqueous solution was used instead of the scandium nitrate aqueous solution, catalysts of the Twentieth Preferred Embodiment were prepared in the same manner as the Nineteenth Preferred Embodiment.

Twenty-first Preferred Embodiment

Except that a lanthanum nitrate aqueous solution was used instead of the scandium nitrate aqueous solution, catalysts of the Twenty-first Preferred Embodiment were prepared in the same manner as the
 5 Nineteenth Preferred Embodiment.

Twenty-second Preferred Embodiment

Except that a neodymium nitrate aqueous solution was used instead of the scandium nitrate aqueous solution, catalysts of the Twenty-second Preferred Embodiment were prepared in the same manner as the
 10 Nineteenth Preferred Embodiment.

Twenty-third Preferred Embodiment

15 (Preparation of $\text{La}_2\text{O}_3\text{-TiO}_2\text{-Al}_2\text{O}_3$ Composite Powder)

In a flask adapted for synthesizing sol-gel and provided with a reflux, 41.2 grams of lanthanum nitrate was dissolved into 3 liters of 2-propanol, and the resulting mixed solution was held at 80 °C. While stirring the mixed solution, 1,225 grams of aluminum isopropoxide was charged into the flask to dissolve, and the
 20 mixed solution was further stirred at 80 °C for 2 hours.

Thereafter, while stirring the mixed solution at 80 °C, 568.4 grams of tetraethyl titanate was dropped into the flask. After dropping all of the tetraethyl titanate, the mixed solution was further kept to be stirred at 80 °C for 2 hours.

Moreover, while stirring the mixed solution at 80 °C, a mixed solution containing 432 grams of pure
 25 water and 2 liters of 2-propanol was dropped. The dropping rate was adjusted to 20 c.c./min. After dropping, the mixed solution was kept to be stirred at 80 °C for 2 hours.

Finally, after aging the thus mixed solution at room temperature for one day and one night, the water content and the alcohol content were removed from the mixed solution by using a rotary evaporator. After naturally drying the resulting residue, the residue was dried forcibly at 110 °C, and it was calcinated at 600
 30 °C for 3 hours. Thus, an $\text{La}_2\text{O}_3\text{-TiO}_2\text{-Al}_2\text{O}_3$ composite powder was produced which had a Ti/Al compositing ratio of 25/75 expressed in molar ratio. In the $\text{La}_2\text{O}_3\text{-TiO}_2\text{-Al}_2\text{O}_3$ composite powder, 0.06 moles of La_2O_3 was included with respect to 120 grams of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder.

Thereafter, a coating layer was formed on a plurality of honeycomb support substrates by using the thus prepared $\text{La}_2\text{O}_3\text{-TiO}_2\text{-Al}_2\text{O}_3$ composite powder, and Pt and Ba were loaded thereon in the same
 35 manner as the Nineteenth Preferred Embodiment. Catalysts of the Twenty-third Preferred Embodiment were thus prepared.

Comparative Example No. 9

40 Except that no scandium nitrate aqueous solution was impregnated to prepare a $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite powder free from Sc_2O_3 , catalysts of Comparative Example No. 9 were prepared in the same manner as the Nineteenth Preferred Embodiment.

Examination and Evaluation

45 Each of the catalysts of the Nineteenth through Twenty-third Preferred Embodiments and Comparative Example No. 9 was disposed in an exhaust line of an actual vehicle equipped with a gasoline engine. The gasoline engine had a displacement of 1.6 liters. The vehicle was driven so as to control the air-fuel ratio A/F at the theoretical value of 14.6, and, at the same time, to vary the temperature of the exhaust gas introduced into the catalysts at a predetermined rate. Thus, the temperature was measured at which the
 50 catalysts exhibited 50% HC conversion.

After the aforementioned examination, each of the catalysts of the Nineteenth through Twenty-third Preferred Embodiments and Comparative Example No. 9 was subjected to a bench test on durability which utilized the same type of engine as above. Namely, each of them was disposed in an exhaust line of the
 55 engine, and then the engine was run for 100 hours while adjusting the temperature of the exhaust gas introduced into them at 800 °C at the theoretical air-fuel ratio A/F of 14.6. After this bench test was over, each of them was again disposed in the exhaust line of the actual vehicle. The vehicle was driven in the same manner as described above, thereby measuring the temperature at which the catalysts exhibited 50%

HC conversion. The results of these examinations are summarized in the columns designated at "Temp. at Initial- 50% HC Conversion" and "Temp. at 50% HC Conversion after Durability Test" in Table 4, respectively.

TABLE 4

	Coating Layer Composition	Pt Loading Amount (grams/liter)	Ba Loading Amount (mole/liter)	Temp. (°C) Initial 50% HC Conversion	Temp. (°C) 50% HC Conversion after Durability Test
19th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ -Sc ₂ O ₃	2.0	0.3	274	336
20th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ -Y ₂ O ₃	2.0	0.3	275	334
21st Pref. Embodiment	TiO ₂ -Al ₂ O ₃ -La ₂ O ₃	2.0	0.3	274	330
22nd Pref. Embodiment	TiO ₂ -Al ₂ O ₃ -Nd ₂ O ₃	2.0	0.3	273	332
23rd Pref. Embodiment	La ₂ O ₃ -TiO ₂ -Al ₂ O ₃	2.0	0.3	270	326
Comp. Ex. No. 9	TiO ₂ -Al ₂ O ₃	2.0	0.3	276	366

It is appreciated from Table 4 that the catalysts of the Nineteenth through Twenty-third Preferred Embodiments degraded in lesser degree in terms of the oxidation activity after a durability test than those of Comparative Example No. 9 did. Thus, the catalysts of the Nineteenth through Twenty-third Preferred Embodiments were found to be improved in durability. Especially, like the catalysts of the Twenty-third Preferred Embodiment, when the compositing of the coating layer is carried out in a highly dispersed state during the sol-gel synthesizing step, it was found that the resulting catalysts are superior to the catalysts of the Twenty-first Preferred Embodiment in which the compositing of La was carried out after the sol-gel synthesizing step.

Note that, however, the exhaust-gases-purifying catalysts of the Nineteenth through Twenty-third Preferred Embodiments as well as those of Comparative Example No. 9 exhibited NO_x purifying performance equivalent to the NO_x purifying performance exhibited by the exhaust-gases-purifying catalysts of the Second Preferred Embodiment.

Twenty-fourth Preferred Embodiment

110 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 40.7 parts of titania sol containing titania in an amount of 30% by weight, 200 parts of water, and 60 parts of a barium carbonate powder were mixed, thereby preparing a slurry for coating.

Then, a plurality of honeycomb support substrates formed of cordierite and having a diameter of 30 mm and a length of 50 mm were immersed into the slurry, and thereafter each of them was blown to blow away the slurry in excess. Each of the support substrates was dried at 80 °C for 20 minutes, and thereafter each of them was calcinated at 600 °C for 1 hour, thereby forming a TiO₂-Al₂O₃ coating layer with Ce and Ba loaded. The coating layer was thus coated on the honeycomb support substrate to include alumina and titania in amounts of 120 grams and 12.2 grams, respectively, with respect to 1 liter of the honeycomb support substrate. The Ti/Al compositing ratio was 6/94 expressed in molar ratio. Each of the Ce and Ba was loaded in an amount of 0.3 moles with respect to 1 liter of the honeycomb support substrate.

Each of the honeycomb support substrates having the coating layer was immersed into a platinum dinitrodiammine aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Pt thereon. Moreover, each of the support substrates with Pt loaded was immersed into a rhodium nitrate aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Rh thereon. The loading amounts of Pt and Rh were 2.0 grams and 0.1 grams, respectively, with respect to 132.2 grams of the TiO₂-Al₂O₃ composite (or 1 liter of the honeycomb support substrate).

Twenty-fifth Preferred Embodiment

Except that 110 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 12.2 parts of a titania powder, 200 parts of water, and 60 parts of a barium carbonate powder were mixed to prepare a slurry for coating, catalysts of the Twenty-fifth Preferred Embodiment were prepared in the same manner as the Twenty-fourth Preferred Embodiment, and they had an identical composition thereto.

Twenty-sixth Preferred Embodiment

When preparing catalysts of the Twenty-sixth Preferred Embodiment, 110 parts of an active alumina powder, 10 parts of a pseudo-boehmite powder, 40.7 parts of titania sol containing 30% by weight of titania, and 200 parts of water were mixed to prepare a slurry for coating. The slurry was coated on each of the honeycomb support substrates in the same manner as the Twenty-fourth Preferred Embodiment. The coating layer was thus coated on the honeycomb support substrate to include alumina and titania in amounts of 120 grams and 12.2 grams, respectively, with respect to 1 liter of the honeycomb support substrate. The Ti/Al compositing ratio was 6/94 expressed in molar ratio.

Each of the honeycomb support substrates having the coating layer was immersed into a cerium nitrate aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Ce thereon. Further, each of the support

substrates with Ce load d was immersed into a platinum dinitrodiammine aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Pt thereon. Furthermore, each of the support substrates with Ce and Pt loaded was immersed into a rhodium nitrate aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Rh thereon. The loading amounts of Pt and Rh were 2.0 grams and 0.1 grams, respectively, with respect to 132.2 grams of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite (or 1 liter of the honeycomb support substrate).

Finally, each of the support substrates with Ce, Pt and Rh loaded was immersed into a barium acetate aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, thereby loading Ba thereon. The loading amounts of Ce and Ba were identical to those of the Twenty-fourth Preferred Embodiment.

Twenty-seventh through Thirty-first Preferred Embodiments

The catalysts of the Twenty-fourth Preferred Embodiment were further immersed into an alkali metal compound aqueous solution or an alkaline-earth metal compound aqueous solution having a predetermined concentration. After taking each of the support substrates out of the aqueous solution, it was blown to blow away the water droplets in excess. After the blowing, each of the support substrates was dried at 250 °C, and it was calcinated at 500 °C for 1 hour. Thus, as set forth in Table 6 below, the alkali metals and the alkaline-earth metals other than Ba were loaded on the support substrates in amounts of 0.1 mole, respectively, with respect to 1 liter of the support substrates, thereby preparing catalysts of the Twenty-seventh through Thirty-first Preferred Embodiments.

Thirty-second Preferred Embodiment

Except that 90 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 30 parts of a titania powder, 200 parts of water, and 60 parts of a barium carbonate powder were mixed to prepare a slurry for coating, catalysts of the Thirty-second Preferred Embodiment were prepared in the same manner as the Twenty-fourth Preferred Embodiment.

In the catalysts of the Thirty-second Preferred Embodiment, the coating layer was thus coated on the honeycomb support substrate to include alumina and titania in amounts of 90 grams and 30 grams, respectively, with respect to 1 liter of the honeycomb support substrate, and the Ti/Al compositing ratio was 7/32 expressed in molar ratio. The Ce and Ba were loaded in amounts of 0.3 moles, respectively, with respect to 1 liter of the honeycomb support substrate. The Pt and Rh were loaded in amounts of 2.0 grams and 0.1 grams, respectively, with respect to 1 liter of the honeycomb support substrate.

Thirty-third Preferred Embodiment

Except that a palladium nitrate aqueous solution was used instead of the platinum dinitrodiammine aqueous solution, and each of the honeycomb support substrates was dried at 80 °C to load Pd, instead of Pt, in an amount of 10 grams with respect to 1 liter of the honeycomb support substrate, catalysts of the Thirty-third Preferred Embodiment were prepared in the same manner as the Twenty-fourth Preferred Embodiment.

Comparative Example No. 10

Except that 110 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 40.7 parts of alumina sol containing alumina in an amount of 30% by weight, 200 parts of water, and 60 parts of a barium carbonate powder were mixed to prepare a slurry for coating, and the coating layer was coated to include alumina in amount of 120 grams with respect to 1 liter of the honeycomb support substrate, catalysts of Comparative Example No. 10 were prepared in the same manner as the Twenty-fourth Preferred Embodiment. Their composition is detailed in Table 6.

Comparative Example No. 11

Except that 110 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 12.2 parts of alumina sol containing alumina in an amount of 30% by weight, 200
 5 parts of water, and 60 parts of a barium carbonate powder were mixed to prepare a slurry for coating, and the coating layer was coated to include alumina in amount of 120 grams with respect to 1 liter of the honeycomb support substrate, catalysts of Comparative Example No. 11 were prepared in the same manner as the Twenty-fourth Preferred Embodiment. Their composition is detailed in Table 6.

10 Comparative Example No. 12

Except that 110 parts of an active alumina powder, 50 parts of a cerium oxide powder, 10 parts of a pseudo-boehmite powder, 40.7 parts of titania sol containing titanic in an amount of 30% by weight and 200
 15 parts of water, but free from a barium carbonate powder, were mixed to prepare a slurry for coating, catalysts of Comparative Example No. 12 were prepared in the same manner as the Twenty-fourth Preferred Embodiment. Their composition is detailed in Table 6.

Examination and Evaluation

20 Each of the catalysts of the Twenty-fourth through Thirty-third Preferred Embodiments and Comparative Example Nos. 10 through 12 was examined for its performance by using model gases. As recited in in Table 5 below, 3 model gases were used to degrade the catalysts, and 2 model gases were used to evaluate the performance of the catalysts. The model gases had the compositions set forth in Table 5. Specifically, each of the catalysts was treated with the model gas equivalent to an A/F ratio of 18 for
 25 degrading at 800 °C for 5 hours. Moreover, at 500 °C, each of them was treated alternately with the model gas equivalent to an A/F ratio of 22 for degrading for 4 minutes, and with the model gas equivalent to an A/F ratio of 14.5 for degrading for 1 minute. This alternating cycle was repeated for 10 hours, thereby carrying out a durability test. During this durability test, the flow of the model gases was adjusted to 1 liter/min., and each of the catalysts was thus forcibly exposed to SO₂.

30 Then, into each of the catalysts subjected to the durability test the model gas equivalent to an A/F ratio of 22 for evaluating and the model gas equivalent to an A/F ratio of 14.5 for evaluating were alternately flowed at 350 °C for 2 minutes. This alternating cycle was repeated for 5 times. When the model gas equivalent to an A/F ratio of 22 for evaluating was flowed, each of the catalysts was examined for average NO_x, CO and HC conversions after a durability test. The results of this examination are also summarized in
 35 Table 6.

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TABLE 5

	A/F	NO	CO	C ₃ H ₆	O ₂	H ₂	SO ₂	H ₂ O	N ₂
	Ratio								
For Degrading	18	-	0.1	0.06	4	-	0.05	6	balance
-ditto-	22	-	0.1	0.12	6	-	0.05	6	balance
-ditto-	14.5	-	0.6	0.04	0.3	0.2	0.05	6	balance
For Evaluating	22	0.05	0.1	0.12	6	-	2 ppm	6	balance
-ditto-	14.5	0.12	0.6	0.04	0.3	0.2	2 ppm	6	balance

(Note) Unless otherwise specified, the unit is %.

TABLE 6

	Coating Layer Ti Composition (Ti/Al Com- positing Ratio)	Addition Form	Noble Metal Catalyst In- gredient Load- ing Amount (gram/liter)	NOx Adsorbent Amount (mole/liter)	Pt	Pd	Rh	Ce	Ba	La	Sr	Li	K	Cs	HC	CO	NOx	Conversion after Durability Test (%)
24th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	55	97	93	
25th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Powder	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	54	96	94	
26th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	55	96	93	
27th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	0.1	-	-	-	-	-	56	97	94	
28th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	0.1	-	-	-	-	54	96	94	
29th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	-	-	0.1	-	-	52	95	94	
30th Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	-	-	-	0.1	-	53	95	91	
31st Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	0.1	56	94	89	
32nd Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (7/32)	Powder	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	57	96	92	
33rd Pref. Embodiment	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	-	10	0.2	0.3	0.3	0.3	-	-	-	-	-	-	52	95	95	
Comp. Ex. No. 10	Al ₂ O ₃	-	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	44	95	93	
Comp. Ex. No. 11	Al ₂ O ₃	-	2	-	0.1	0.3	0.3	0.3	-	-	-	-	-	-	43	95	93	
Comp. Ex. No. 12	TiO ₂ -Al ₂ O ₃ (6/94)	Sol	2	-	0.1	0.3	-	-	-	-	-	-	-	-	35	96	95	

In the catalysts of the Twenty-fourth through Thirty-third Preferred Embodiments, since the coating layer was formed of the TiO₂-Al₂O₃ composite, they exhibited the high NO_x conversion of more than 50% even after a durability test. Moreover, in the catalysts of the Twenty-fourth, Twenty-fifth, Thirty-second and Thirty-third Preferred Embodiments, there was possibility that at least one of Ce and Ba was further composited with the TiO₂-Al₂O₃ composite.

On the other hand, in the catalysts of Comparative Example Nos. 10 and 11, the coating layer was formed of the simple Al_2O_3 . Even if Ce was composited with Al_2O_3 to form an $\text{Al}_2\text{O}_3\text{-CeO}_2$ composite, the composite does not satisfy the limitation of the present invention recited in the accompanying claims. That is, the catalysts of Comparative Example Nos. 10 and 11 adsorbed the SO_x , and they exhibited the deteriorated NO_x conversion after a durability test.

In addition, in the catalysts of Comparative Example No. 12, although the coating layer was formed of the $\text{TiO}_2\text{-Al}_2\text{O}_3$ composite, no NO_x adsorbent was loaded thereon. Thus, they exhibited the considerably degraded NO_x conversion after a durability test.

In particular, it is appreciated from the catalysts of the Twenty-fourth through Thirty-third Preferred Embodiments revealed that the composite support according to the present invention can be formed not only by the sol-gel process but also by mixing and calcinating a powder and sol or by mixing and calcinating powders.

Having now fully described the present invention, it will be apparent to one of ordinary skill in the art that many changes and modifications can be made thereto without departing from the spirit or scope of the present invention as set forth herein including the appended claims.

Claims

1. A catalyst for purifying exhaust gases, comprising:
 - a support including at least one composite selected from the group consisting of $\text{TiO}_2\text{-Al}_2\text{O}_3$, $\text{ZrO}_2\text{-Al}_2\text{O}_3$ and $\text{SiO}_2\text{-Al}_2\text{O}_3$ composites;
 - an NO_x adsorbent including at least one member selected from the group consisting of alkali metals, alkaline-earth metals and rare-earth elements, and loaded on said support; and
 - a noble metal catalyst ingredient loaded on said support.
2. The catalyst according to Claim 1, wherein said support includes at least one of TiO_2 , ZrO_2 and SiO_2 - (hereinafter collectively referred to as MO_2), and Al_2O_3 so as to satisfy the following compositing ratio, defined by moles of their metallic components, of MO_2 with respect to Al_2O_3 :

$$\text{M/Al} = 5/95 \text{ through } 50/50.$$
3. The catalyst according to Claim 2, wherein the compositing ratio M/Al falls in a range of from 20/80 to 30/70.
4. The catalyst according to Claim 1, wherein said support includes the $\text{SiO}_2\text{-Al}_2\text{O}_3$ composite so as to satisfy the following compositing ratio, defined by moles of metallic components of SiO_2 and Al_2O_3 , of SiO_2 with respect to Al_2O_3 :

$$\text{Si/Al} = 4/96 \text{ through } 20/80.$$
5. The catalyst according to Claim 4, wherein the compositing ratio Si/Al falls in a range of from 4/96 to 15/85.
6. The catalyst according to Claim 1, wherein said NO_x adsorbent is at least one alkali metal selected from the group consisting of lithium (Li), sodium (Na), potassium (K), rubidium (Rb), cesium (Cs) and francium (Fr).
7. The catalyst according to Claim 1, wherein said NO_x adsorbent is at least one alkaline-earth metal selected from the group consisting of barium (Ba), beryllium (Be), magnesium (Mg), calcium (Ca) and strontium (Sr).
8. The catalyst according to Claim 1, wherein said NO_x adsorbent is at least one rare-earth element selected from the group consisting of scandium (Sc), yttrium (Y), lanthanum (La), cerium (Ce), praseodymium (Pr) and neodymium (Nd).
9. The catalyst according to Claim 1, wherein said NO_x adsorbent is loaded in an amount which is effective to adsorb nitrogen oxide (NO_x) in exhaust gases whose oxygen concentrations are at the stoichiometric point or more than required for oxidizing carbon monoxide (CO) and hydrocarbons (HC).

10. The catalyst according to Claim 9, wherein said NO_x adsorbent is loaded in amount of from 0.05 to 1.0 mole with respect to 120 grams of said support.
11. The catalyst according to Claim 1, wherein said noble metal catalyst ingredient is at least one element selected from the group consisting of Pd, Rh and Pd.
12. The catalyst according to Claim 1, wherein said noble metal catalyst ingredient is loaded in an amount which is effective to purify NO_x, CO and HC in exhaust gases whose oxygen concentrations are at the stoichiometric point or more than required for oxidizing CO and HC.
13. The catalyst according to Claim 12, wherein said noble metal catalyst ingredient is at least one element selected from the group consisting of Pd and Pd, and loaded in an amount of from 0.1 to 20.0 grams with respect to 120 grams of said support.
14. The catalyst according to Claim 13, wherein said noble metal catalyst ingredient is loaded in an amount of from 0.5 to 10.0 grams with respect thereto.
15. The catalyst according to Claim 12, wherein said noble metal catalyst ingredient is Rh, and loaded in an amount of from 0.01 to 80.0 grams with respect to 120 grams of said support.
16. The catalyst according to Claim 15, wherein said noble metal catalyst ingredient is loaded in an amount of from 0.05 to 5.0 grams with respect thereto.
17. A catalyst for purifying exhaust gases, comprising:
 - a composite support including TiO₂, Al₂O₃, and at least one element selected from the group consisting of alkaline-earth metals and rare-earth elements;
 - an NO_x adsorbent including at least one member selected from the group consisting of alkali metals, alkaline-earth metals and rare-earth elements, and loaded on said composite support; and
 - a noble metal catalyst ingredient loaded on said composite support.
18. The catalyst according to Claim 17, wherein said composite support includes TiO₂ and Al₂O₃ so as to satisfy the following compositing ratio, defined by moles of metallic components of TiO₂ and Al₂O₃, of TiO₂ with respect to Al₂O₃:

Ti/Al = 5/95 through 50/50.
19. The catalyst according to Claim 18, wherein the compositing ratio Ti/Al falls in a range of from 20/80 to 30/70.
20. The catalyst according to Claim 17, wherein said NO_x adsorbent is at least one alkali metal selected from the group consisting of lithium (Li), sodium (Na), potassium (K), rubidium (Rb), cesium (Cs) and francium (Fr).
21. The catalyst according to Claim 17, wherein said NO_x adsorbent is at least one alkaline-earth metal selected from the group consisting of barium (Ba), beryllium (Be), magnesium (Mg), calcium (Ca) and strontium (Sr).
22. The catalyst according to Claim 17, wherein said NO_x adsorbent is at least one rare-earth element selected from the group consisting of scandium (Sc), yttrium (Y), lanthanum (La), cerium (Ce), praseodymium (Pr) and neodymium (Nd).
23. The catalyst according to Claim 17, wherein said NO_x adsorbent is loaded in an amount which is effective to adsorb nitrogen oxide (NO_x) in exhaust gases whose oxygen concentrations are at the stoichiometric point or more than required for oxidizing carbon monoxide (CO) and hydrocarbons (HC).
24. The catalyst according to Claim 23, wherein said NO_x adsorbent is loaded in amount of from 0.05 to 1.0 mole with respect to 120 grams of said composite support.

25. The catalyst according to Claim 17, wherein said noble metal catalyst ingredient is at least one element selected from the group consisting of Pd, Rh and Pd.
- 5 26. The catalyst according to Claim 17, wherein said noble metal catalyst ingredient is loaded in an amount which is effective to purify NO_x, CO and HC in exhaust gases whose oxygen concentrations are at the stoichiometric point or more than required for oxidizing CO and HC.
- 10 27. The catalyst according to Claim 26, wherein said noble metal catalyst ingredient is at least one element selected from the group consisting of Pd and Pd, and loaded in an amount of from 0.1 to 20.0 grams with respect to 120 grams of said composite support.
28. The catalyst according to Claim 27, wherein said noble metal catalyst ingredient is loaded in an amount of from 0.5 to 10.0 grams with respect thereto.
- 15 29. The catalyst according to Claim 26, wherein said noble metal catalyst ingredient is Rh, and loaded in an amount of from 0.01 to 80.0 grams with respect to 120 grams of said composite support.
- 20 30. The catalyst according to Claim 29, wherein said noble metal catalyst ingredient is loaded in an amount of from 0.05 to 5.0 grams with respect thereto.



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EUROPEAN SEARCH REPORT

Application Number
EP 94 11 9311

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
P,X	EP-A-0 613 714 (TOYOTA JIDOSHA KK) 7 September 1994 * page 3, line 48 - page 6, line 52; claims 1-16 *	1,6-16	B01D53/94 B01J23/56 B01J23/58
X	EP-A-0 507 590 (NIPPON SHOKUBAI CO. LTD.) * page 5, line 9 - line 40; claims 1-13 *	1-5, 7-19, 21-30	
X	EP-A-0 485 180 (MGK INSULATORS LTD.) * page 4, line 49 - page 5, line 56; claims 1-17 *	1,7-17, 21-30	
X	EP-A-0 372 156 (NIPPON SHOKUBAI CO. LTD.) * page 2, line 54 - page 4, line 39; claims 1-11 *	1,6, 8-17,20, 22-30	
X	EP-A-0 558 159 (NIPPON SHOKUBAI CO. LTD.) * page 2, line 36 - page 3, line 54 *	1,7-16	TECHNICAL FIELDS SEARCHED (Int.Cl.6) B01D B01J
X	EP-A-0 562 516 (TOYOTA JIDOSHA KK ET AL.) * page 3, line 40 - page 6, line 3; claims 1-7 *	1,7-14	
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 6 March 1995	Examiner Eijkenboom, A
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document Y : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document			